

# RIVERS AND STREAMS

Compilation by B. Cushman-Roisin  
Dartmouth College

## 1. Flow:

River parameters are:

$$S = \text{slope of river bed} = \frac{\text{vertical drop}}{\text{downstream distance}}$$

$$A = \text{cross-sectional area of flowing water}$$

$P$  = wetted perimeter = bottom contour length from shoreline to opposite shoreline

$$W = \text{river width} = \text{surface distance from shoreline to opposite shoreline}$$

$$H = \text{average water depth} = \frac{A}{W}$$

$$g = \text{gravitational acceleration} = 9.81 \text{ m/s}^2$$

$$\rho = \text{water density} = 1000 \text{ kg/m}^3$$

From these parameters, determine:

$$R_h = \text{hydraulic radius} = \frac{A}{P}$$

$$u_* = \text{turbulent (friction) velocity} = \sqrt{gR_h S}$$

$$\bar{u} = \text{average velocity} = C u_* = C \sqrt{gR_h S} \text{ (Chézy formula)}$$

For a wide and shallow river,  $R_h$  is nearly equal to  $H$ , and  $H$  can be substituted for  $R_h$  in the formulas.

Manning's formula:

$$C\sqrt{g} = \frac{R_h^{1/6}}{n},$$

with  $R_h$  in meters and  $C$  dimensionless. Typical values for  $n$  range from 0.012 for a very smooth channel to 0.150 for a very rough and meandering river bed.

If a value of  $n$  is not specified, take  $n = 0.035$ .

**2. Manning's factor:**

| Channel type      |                       | <i>n</i> |
|-------------------|-----------------------|----------|
| Cement            | smooth slabs          | 0.012    |
|                   | finished              | 0.014    |
|                   | unfinished            | 0.014    |
|                   | bottom sand ripples   | 0.018    |
|                   | very rough            | 0.020    |
| Asphalt           |                       | 0.016    |
| Excavated channel | clay loam             | 0.018    |
|                   | gravel                | 0.025    |
|                   | weeds                 | 0.030    |
|                   | cobbles               | 0.030    |
|                   | stones                | 0.035    |
| Natural channel   | cobblestone bed       | 0.030    |
|                   | irregular edges       | 0.035    |
|                   | major rivers          | 0.035    |
|                   | rocky edges           | 0.040    |
|                   | sluggish, pools       | 0.040    |
|                   | variable section      | 0.040    |
|                   | irregular, rocks      | 0.045    |
|                   | very irregular, trees | 0.060    |
| Flood plains      | pasture, farmland     | 0.035    |
|                   | light brush           | 0.050    |
|                   | floodway channel      | 0.125    |
|                   | trees, obstructions   | 0.150    |

### 3. Mixing:

Vertical diffusivity (top to bottom mixing):

$$D_{\text{vertical}} = 0.067u_*H$$

Transverse diffusivity (left to right mixing):

$$D_{\text{transverse}} = 0.15u_*H$$

Longitudinal diffusivity (downstream mixing):

$$D_{\text{longitudinal}} = 0.0197 \frac{\bar{u}^2 H}{u_*}$$

or

$$D_{\text{longitudinal}} = 0.011 \frac{\bar{u}^2 W^2}{u_* H}$$

whichever is largest.

Time for vertical homogenization (if discharge is placed at mid-depth):

$$t_{\text{vertical}} = 0.134 \frac{H^2}{D_{\text{vertical}}} = 2.0 \frac{H}{u_*}$$

Quadruple this value if the discharge occurs on the surface or bottom.

Distance for vertical homogenization (if discharge is placed at mid-depth):

$$x_{\text{vertical}} = \bar{u}t_{\text{vertical}} = 2.0 \frac{\bar{u}H}{u_*}$$

Time for transverse homogenization (if discharge is placed along the side):

$$t_{\text{transverse}} = 0.536 \frac{W^2}{D_{\text{transverse}}} = 3.6 \frac{W^2}{u_* H}$$

Distance for transverse homogenization:

$$x_{\text{transverse}} = \bar{u}t_{\text{transverse}} = 3.6 \frac{\bar{u}W^2}{u_* H}$$

#### 4. Re-aeration:

4a) The exchange coefficient of oxygen across the air-sea interface (= vertical transfer velocity, the so-called 'piston velocity') is:

$$k_{O_2}(\text{at } 20^\circ\text{C}) = 3.9 \sqrt{\frac{\bar{u}}{H}},$$

where  $\bar{u}$  is in m/s,  $H$  is in m, and  $k_{O_2}$  is in m/day.

4b) Temperature correction:

$$k_{O_2}(T) = k_{O_2}(20^\circ\text{C}) (1.024)^{T-20},$$

where  $T$  is the ambient temperature in  $^\circ\text{C}$ .

4c) Re-aeration rate:

$$K_{O_2}(T) = \frac{k_{O_2}}{H} = \frac{3.9}{H} \sqrt{\frac{\bar{u}}{H}} (1.024)^{T-20},$$

in 1/day, with  $\bar{u}$  in m/s,  $H$  in m, and  $T$  in  $^\circ\text{C}$ .

#### 5. Biodegradation rates:

- Raw sewage:  $K_{BOD} = 0.35$  to  $0.70$  /day at  $20^\circ\text{C}$
- Treated sewage:  $K_{BOD} = 0.12$  to  $0.23$  /day at  $20^\circ\text{C}$
- Various chemicals: See Masters' book, Table 2-3, page 55

Temperature correction:

$$K_{BOD}(T) = K_{BOD}(20^\circ\text{C}) (1.047)^{T-20},$$

where  $T$  is the ambient temperature in  $^\circ\text{C}$ .